



DAKOTA 101: Calibration

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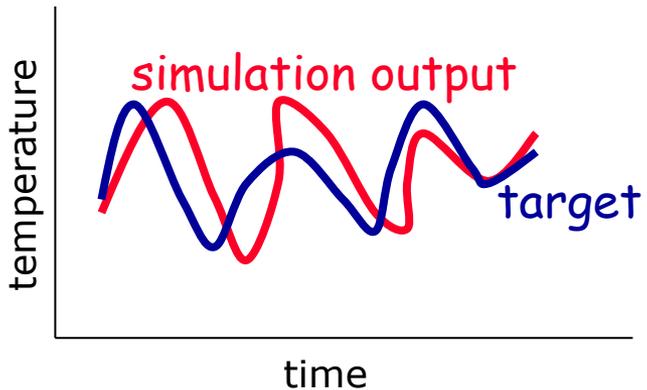


Learning Goals - Calibration



- **Define a calibration/parameter estimation problem**
- **Understand relationship to optimization**
- **Recognize differences in DAKOTA interface**
- **Identify problems in your field**
- **Calibrate cantilever beam model to synthetic data**
- **Become cognizant of potential challenges**

Why Use Calibration?

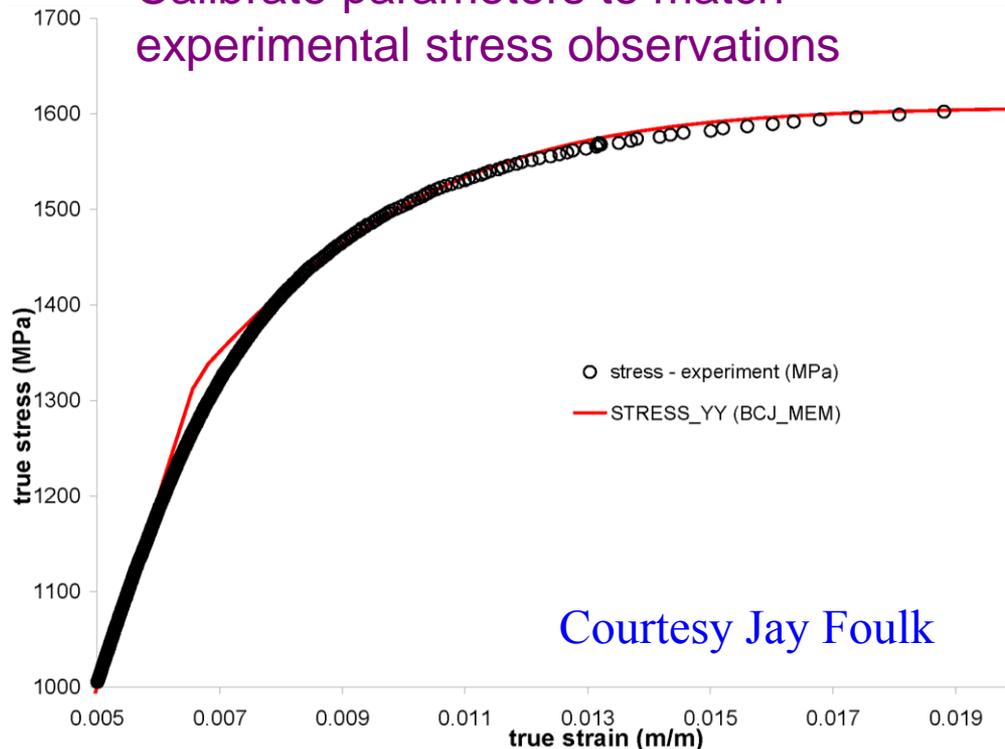


- **What: Determine parameter values that maximize agreement between simulation response and target response**
 - A.K.A. parameter estimation, parameter identification, systems identification, nonlinear least-squares, inverse problem.
 - **Calibration is not validation!** Separate data should be used to assess whether a calibrated model is valid.
- **Why?**
 - **Fit a model to data**
 - E.g., determine material model parameters such that predicted stress-strain curve matches one generated experimentally
 - **Find control settings that enable a system to achieve a prescribed performance profile**
 - E.g., determine thermostat settings the yield uniform building temperature across multiple control zones
 - **Determine source terms for an observed phenomenon**
 - E.g., determine the size and location of a chemical release

Parameter estimation for a material plasticity model



Calibrate parameters to match experimental stress observations



f – yields rate dependence (fit)
 Y – the yield stress (chosen)
 n – exponent in flow rule (fit)
 H – hardening in evolution of κ (fit)
 R_d – recovery in evolution of κ (fit)

f	4.52×10^4
Y	1325 MPa
n	0.386
H	1.10×10^5 MPa
R_d	389

NOTE: Experimental data taken from a representative test, ph13-8-h950-test-3

Flow rule concentrating the effective stress

$$\dot{\epsilon}_p = f \left\{ \sinh \left[\frac{\bar{\sigma}}{(1-\phi)(\kappa+Y)} - 1 \right] \right\}^n$$

evolution of isotropic hardening

$$\dot{\kappa} = [H - R_d \kappa] \dot{\epsilon}_p$$

*Large values of f make the formulation rate independent. I did not need to fit f .

Brief Group Discussion: Calibration Practice



5-10 min discussion

- **In what settings do you have desired model responses or data?**
- **How do you measure differences between target and model response?**
- **How do you go about identifying parameter values that maximize agreement?**
- **What makes your problems challenging?**

Recall the Optimization Problem



Minimize: $f(x_1, \dots, x_N)$

Objective function(s)

Subject to: $g_{LB} \leq g(x) \leq g_{UB}$
 $h(x) = h_E$

Nonlinear inequality constraints

Nonlinear equality constraints

$A_I x \leq b_I$

Linear inequality constraints

$A_E x = b_E$

Linear equality constraints

$x_{LB} \leq x \leq x_{UB}$

Bound constraints

Calibration: Optimization Problem with Special Structure and Goals



Simulation-generated
response

Target response

Minimize: $f(x_1, \dots, x_N) = \sum_{i=1}^m [s_i(x_1, \dots, x_N) - d_i]^2$ *Objective function(s)*

Subject to: $g_{LB} \leq g(x) \leq g_{UB}$
 $h(x) = h_E$

Nonlinear inequality constraints
Nonlinear equality constraints

$A_I x \leq b_I$
 $A_E x = b_E$

Linear inequality constraints
Linear equality constraints

$x_{LB} \leq x \leq x_{UB}$

Bound constraints

DAKOTA Calibration Interface Accommodates Special Structure



Responses Option1: Compute list of these differences (residuals) and return it to DAKOTA. It will square and sum them.

OR

$$\sum_{i=1}^m [s_i(x_1, \dots, x_N) - d_i]^2$$

The equation is annotated with red lines: a bracket above the entire expression, an arrow pointing to the summation index $i=1$, and an arrow pointing to the target response d_i .

Responses Option 2:
Compute list of simulation
responses and...

AND

...tell DAKOTA where to find a data file
with a list of the target responses. It
will put the pieces together.

Local Least-squares Methods Take Advantage of Special Structure



Alternate objective formulation: $f(x) = \frac{1}{2} r(x)^T r(x) = \frac{1}{2} [s(x) - d]^T [s(x) - d]$

Derivative formulations:

$$\nabla f(x) = J(x)^T r(x); \quad J_{ij} = \frac{\partial r_i}{\partial x_j} \quad \nabla^2 f(x) = J^T J + \sum_{i=1}^n r_i(x) \nabla^2 r_i(x)$$

Methods vary in second derivative approximation:

Gauss-Newton: $J(x)^T J(x)$

Levenberg-Marquardt: $J(x)^T J(x) + \mu I$, with $\mu \geq 0$

NL2SOL: $J(x)^T J(x) + S$,

with $S = 0$ or $S =$ Quasi-Newton approximation to $\sum_{i=1}^n f_i(x) \nabla^2 f_i(x)$

Exercise: Calibrate Cantilever to Experimental Data



- Calibrate design variables E , w , t to data from all 3 responses
- X , Y , R fixed (state) at nominal values
- Use NL2SOL or OPT++ Gauss-Newton
- Key DAKOTA specs:
 - `num_least_squares_terms = 3`
 - no constraints
 - `least_squares_datafile`
- Possible template: Calib. Local Data File

DATA	clean	with error
area	7.5	7.772
stress	2667	2658
displacement	0.309	0.320

`cantilever_clean.dat`
`cantilever_witherror.dat`

- *For least-squares methods, application normally must return residuals $r_i(\mathbf{x}) = s_i(\mathbf{x}) - d_i$ to DAKOTA*
- *Here we return the usual area, stress, displacement and specify a datafile and DAKOTA computes the residuals*

Potential Solution: Cantilever Least-Squares



```
# Calibrate to area, stress, and displacement data generated with  
# E = 2.85e7, w = 2.5, t = 3.0
```

```
method
```

```
  nl2sol
```

```
    convergence_tolerance = 1.0e-6
```

```
variables
```

```
  continuous_design = 3
```

```
    upper_bounds  3.1e7 10.0 10.0
```

```
    initial_point 2.9e7 4.0  4.0
```

```
    lower_bounds  2.7e7 1.0  1.0
```

```
    descriptors   'E' 'beam_width' 'beam_thickness'
```

```
# Fix at nominal
```

```
  continuous_state = 3
```

```
    initial_state 40000 500 1000
```

```
    descriptors   'R' 'X' 'Y'
```

```
interface
```

```
  direct
```

```
    analysis_driver = 'mod_cantilever'
```

```
responses
```

```
  calibration_terms = 3
```

```
#   calibration_data_file = 'cantilever_clean.dat'
```

```
     calibration_data_file = 'cantilever_witherror.dat'
```

```
     descriptors = 'area' 'stress' 'displacement'
```

```
  analytic_gradients
```

```
  no_hessians
```

CIs without error:

```
E: [ 2.850e+07, 2.850e+07 ]
```

```
w: [ 2.500e+00, 2.500e+00 ]
```

```
t: [ 3.000e+00, 3.000e+00 ]
```

CIs with error:

```
E: [ 1.992e+07, 4.190e+07 ]
```

```
w: [ 1.962e+00, 3.918e+00 ]
```

```
t: [ 1.954e+00, 3.309e+00 ]
```

Brief Group Discussion: Cantilever Problem and Solution



5-10 min discussion

- How do the calibrated parameter values differ with clean vs. noisy data?
- How do the confidence intervals differ?
- What would you do if you wanted to calibrate against multiple sets of data?
- What would you do if agreement was more important in some regions than others?
- Do you expect that desired target responses always give rise to unique matching parameters?

Quick Guide for Calibration Method Selection



Category	DAKOTA method names	Continuous Variables	Categorical/ Discrete Variables	Bound Constraints	General Constraints
Gradient-Based Local (Smooth Response)	<code>n12sol</code>	X		X	
	<code>n1ssol_sqp</code> , <code>optpp_g_newton</code>	X		X	X
Gradient-Based Global (Smooth Response)	<code>hybrid strategy</code> , <code>multi_start strategy</code>	X		X	X
Derivative-Free Local (Nonsmooth Response)					
Derivative-Free Global (Nonsmooth Response)	<code>efficient_global</code> , <code>surrogate_based_global</code>	X		X	X

See Usage Guidelines in DAKOTA User's Manual. Also, can apply any optimizer when doing derivative-free local or global calibration.

Calibration References



- **G. A. F. Seber and C. J. Wilde, “Nonlinear Regression”, John Wiley and Sons, Inc., Hoboken, New Jersey, 2003.**
- **M. C. Hill and C. R. Tiedeman, “Effective Groundwater Model Calibration: With Analysis of Data, Sensitivities, Predictions, and Uncertainty”, John Wiley and Sons, Inc., Hoboken, New Jersey, 2007.**
- **R. C. Aster, B. Borchers, and C. H. Thurber, “Parameter Estimation and Inverse Problems”, Elsevier, Inc., Oxford, UK, 2005.**
- **DAKOTA User’s Manual**
 - **Nonlinear Least Squares Capabilities**
 - **Surrogate-Based Minimization**
- **DAKOTA Reference Manual**

Learning Goals Revisited: Did we meet them?



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